

Reservoir Simulation of CO₂ Storage in Deep Saline Aquifers



**Presented by:
Mark H. Holtz**

Authors

**A. Kumar, M. Noh, G.A. Pope, K. Sepehrnoori,
S.L. Bryant and L.W. Lake.**

**Center of Petroleum & Geosystems Engineering,
The University of Texas at Austin.**

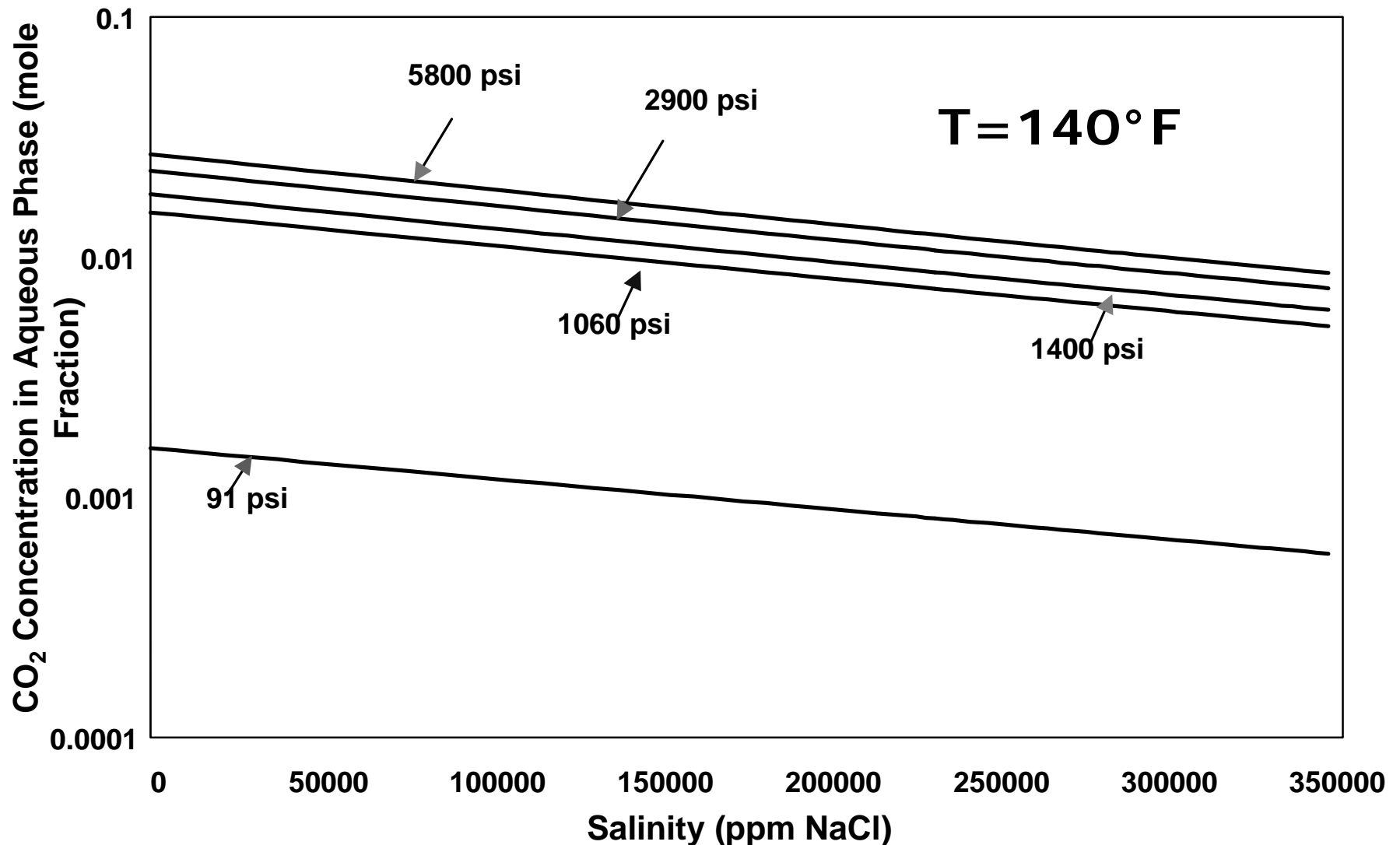
Modeling Approach

- Numerical compositional simulation
- Key processes
 - CO₂/brine mass transfer
 - Multiphase flow
 - During injection (*pressure driven*)
 - After injection (*gravity driven*)
 - Chemical reactions
- Key outputs..CO₂ concentration in
 - Brine (as CO₃²⁻ and HCO₃⁻)
 - Gas (as CO₂)
 - Solid (as CO₃²⁻)

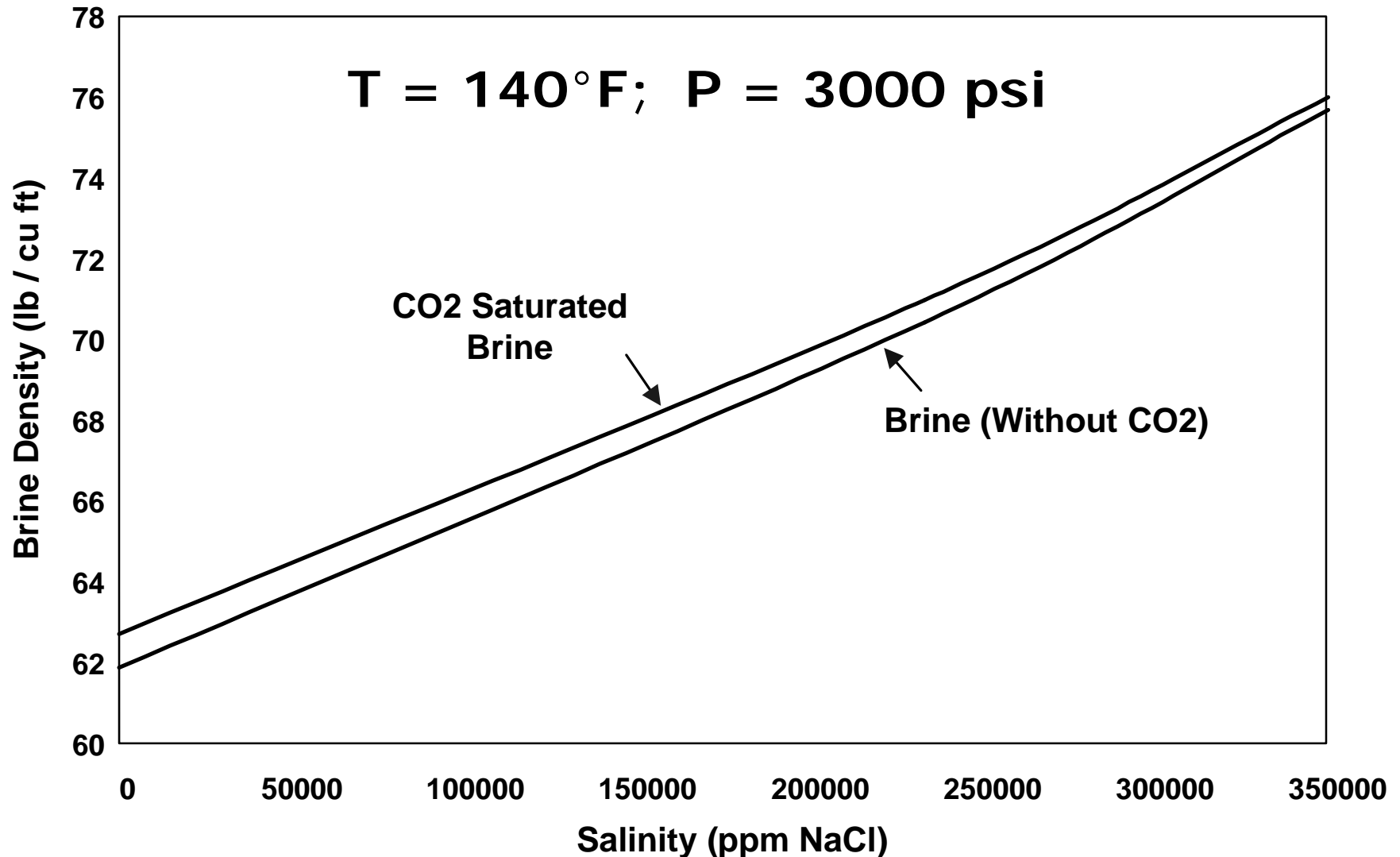
Method

- Obtain/parameterize physical property data
- Numerical simulations of storage scenario
 - 50 years CO₂ injection
 - 1000 years of gravity-driven fluid movement
 - GEM compositional simulator (CMG)
- Quantify storage in different sinks
 - CO₂-rich gas phase (residual saturation)
 - CO₂-saturated brine
 - Carbonate minerals

Key Physical Properties (1): CO₂ Solubility in Aqueous Phase



Key Physical Properties (2): Density of CO₂-Saturated Brine



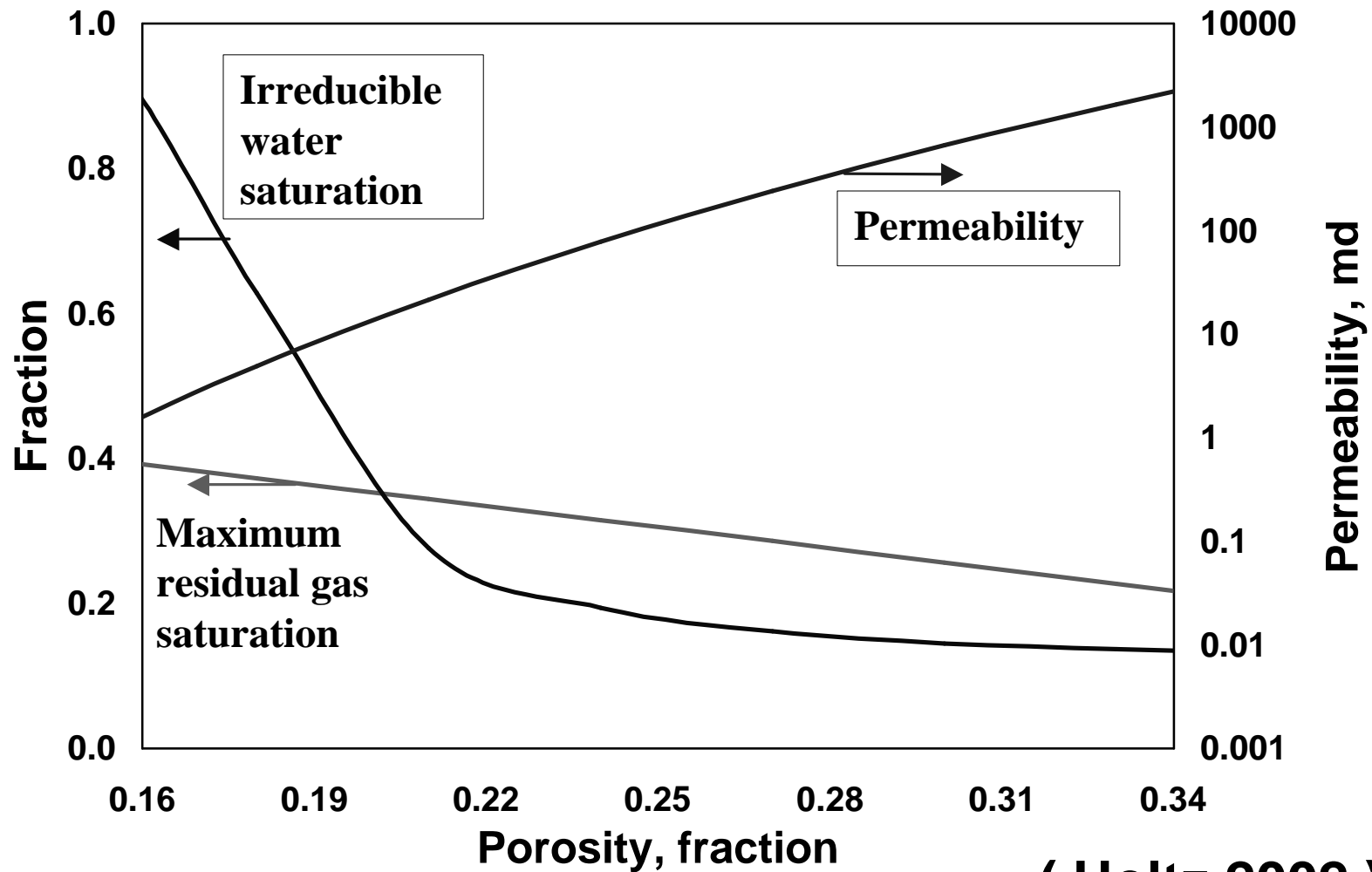
Effects of Physical Properties

- Shallow and high salinity aquifers will dissolve less CO₂ in aqueous phase than deep, low salinity aquifer
 - Salinity affects the distribution of CO₂ between various immobile phases in the order of 10% of total CO₂ injected
- After CO₂ injection ends, buoyancy continues to drive flow
 - Low density CO₂-rich gas will move up
 - High density brine containing dissolved CO₂ will sink

Key Petrophysical Properties

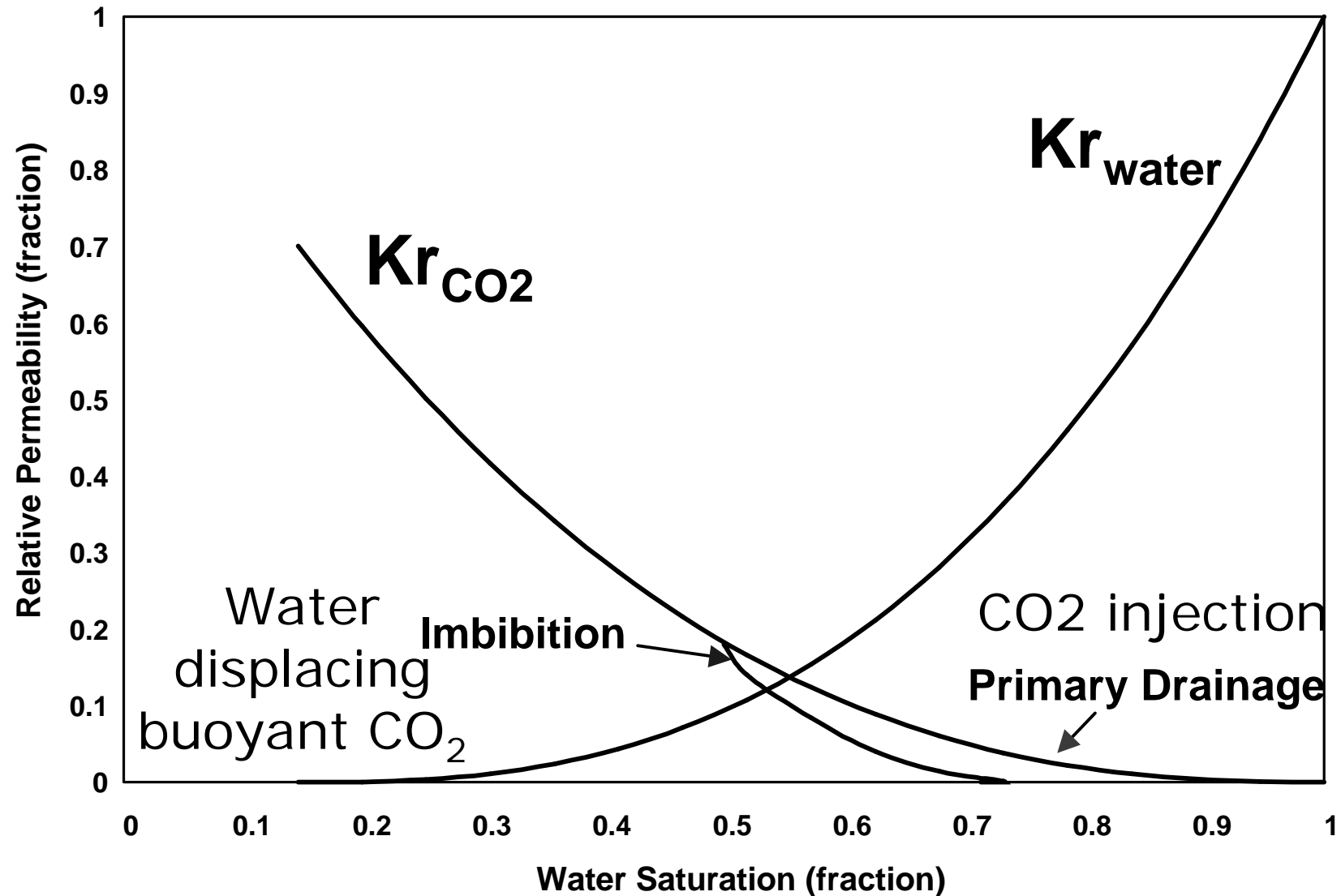
- Porosity
- Permeability
 - Magnitude
 - Anisotropy
- Residual gas saturation
 - Correlation with porosity (Holtz, 2002)
- Relative permeability
- Hysteresis
 - Land model

Correlation Between Various Aquifer Properties



- (Holtz 2002)

Hysteresis during Storage



Modeling Hysteresis with GEM **CPGE** for Gas Relative Permeability Curve

- $k_{rg}(S_g) = k_{rg}(D_r; S_g)$, during drainage;
- $k_{rg}(S_g) = k_{rg}(D_r; S_g(\text{shifted}))$, during imbibition;

where

- $S_g(\text{shifted}) = (S_g - S_{grh})(S_{gh}) / (S_{gh} - S_{grh})$.

$$\frac{1}{S_{gr}^{\max}} - 1 = \frac{1}{S_{grh}} - \frac{1}{S_{gh}}$$

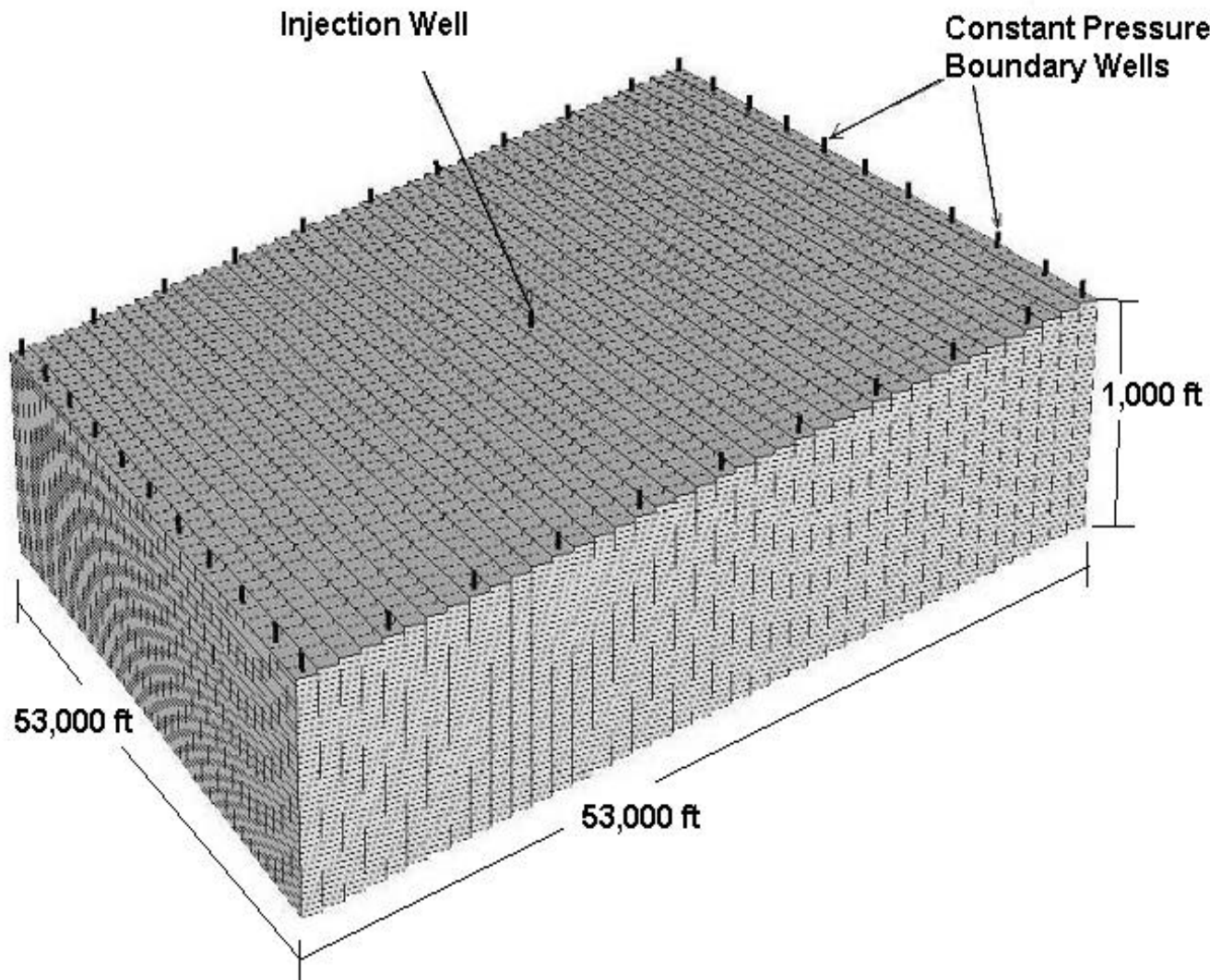
- S_{gh} is the value of S_g when the shift to imbibition occurs
- S_{grh} is the value of S_{gr} corresponding to S_{gh} via Land's equation
- S_{grmax} is the user-entered parameter

Curves

Base Case Simulation



Aquifer and Well Locations





Description of Base Case

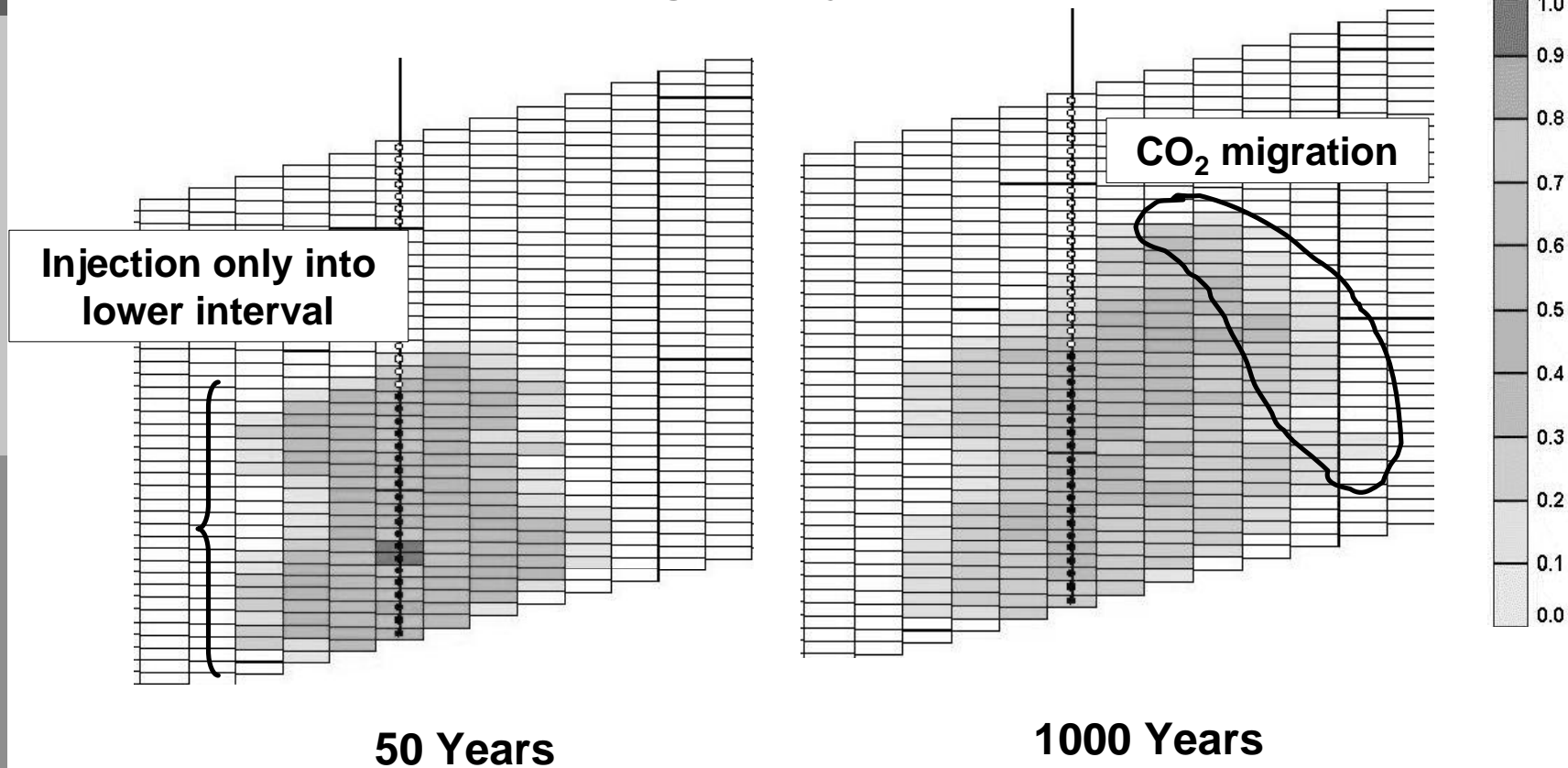
Aquifer Dimensions	53,000 ft x 53,000 ft x 1000 ft
Grid	40 x 40 x 40
Initial Pressure	2265 psi
Aquifer Temperature	140 °F
Mean Permeability	100 md
Permeability Ratio (K_v / K_h)	0.001
Dip	1 degree
Depth	5300 ft
Initial Water Saturation	1.0
Salinity	100,000 ppm
Maximum Injection Pressure	3300 psi
Maximum Injection Rate	50 MMSCF/D
Injection Time	50 years
Total Run Time	1000 years

Results:



Injection Strategy Limits Upward Migration

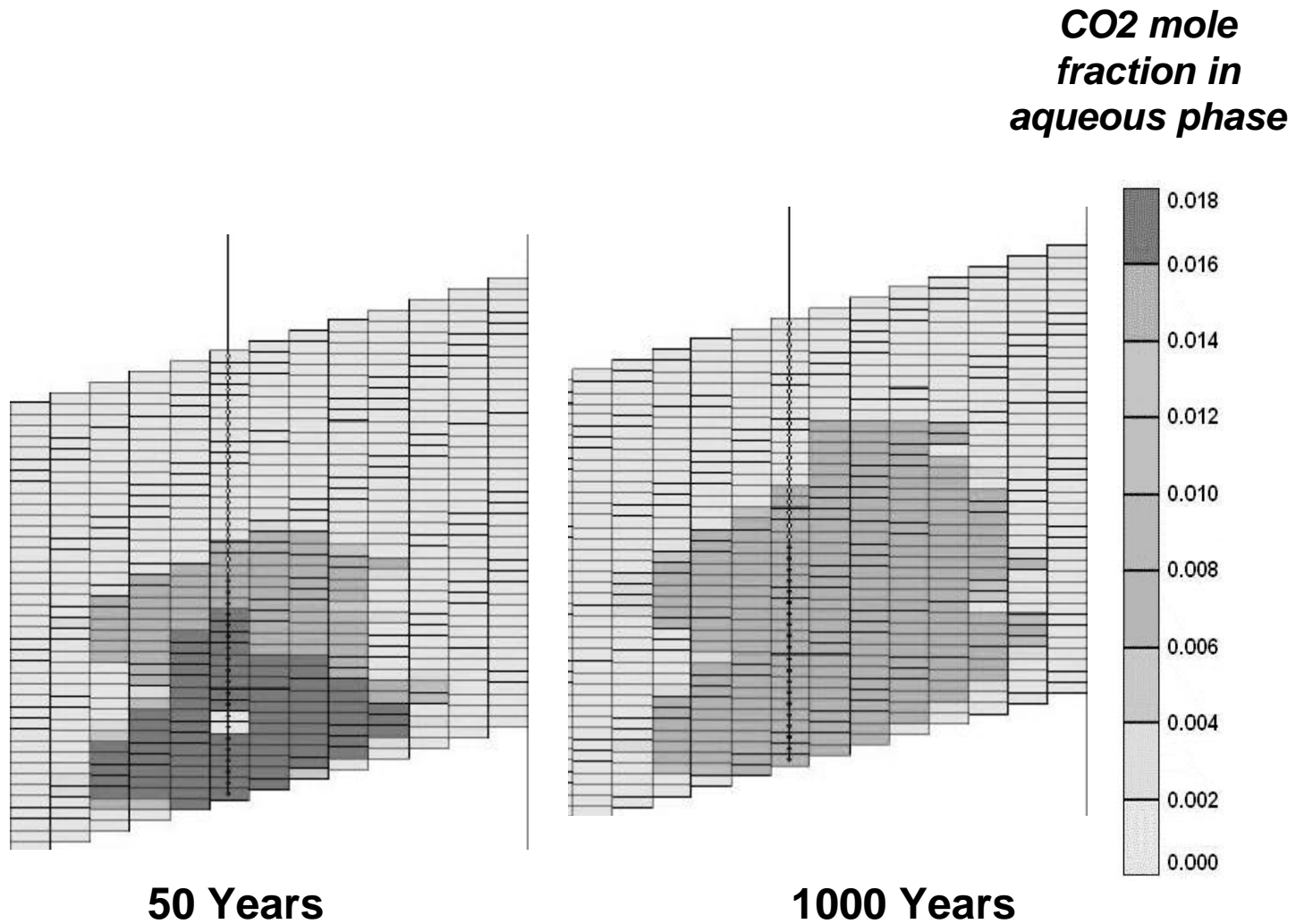
CO₂ phase Saturation Profiles
(vertical slice through the injection well in X-Z direction)



Results:



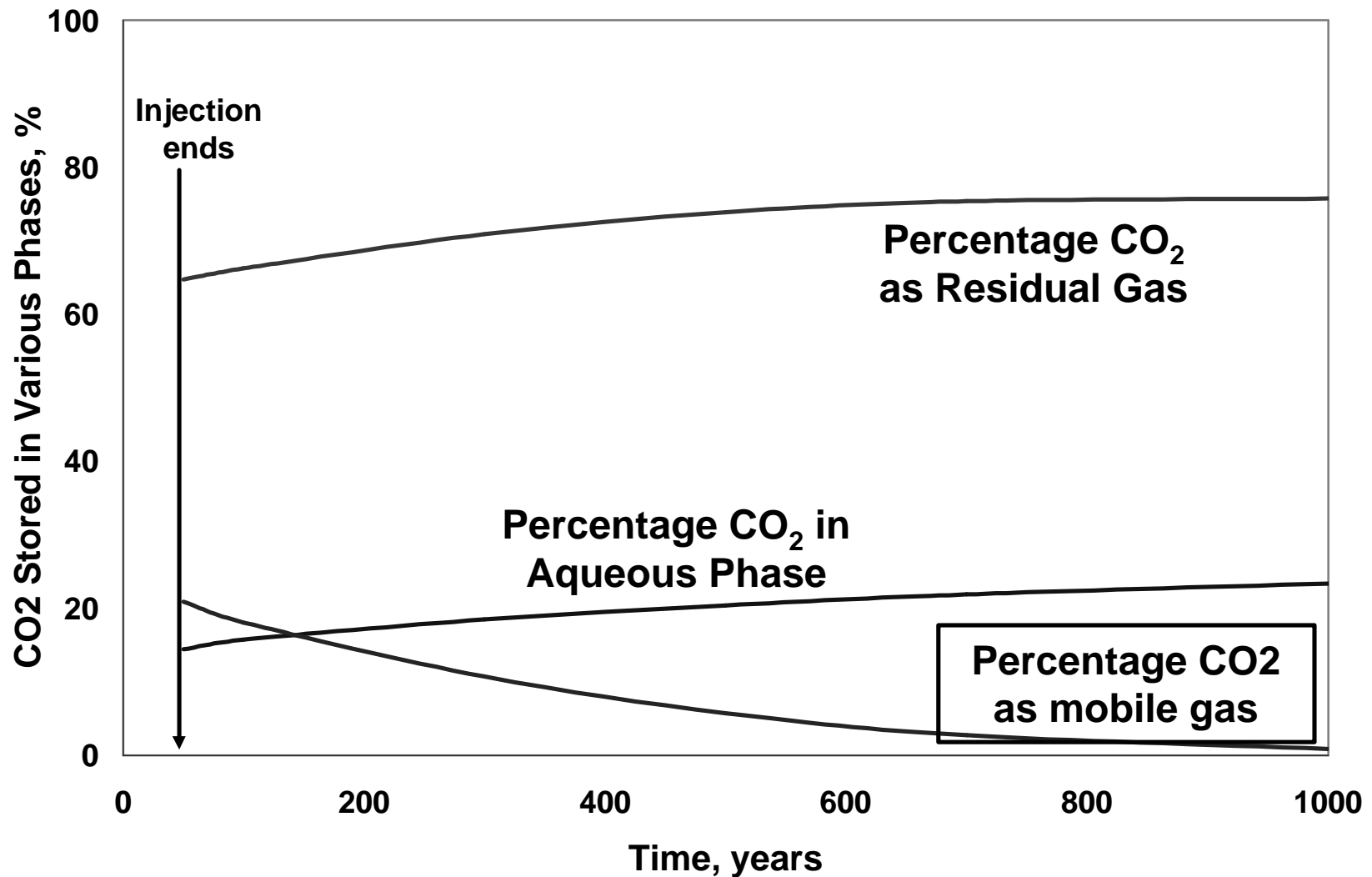
Brine Dissolution concentration migrates up-dip
after injection



Key Findings (1):



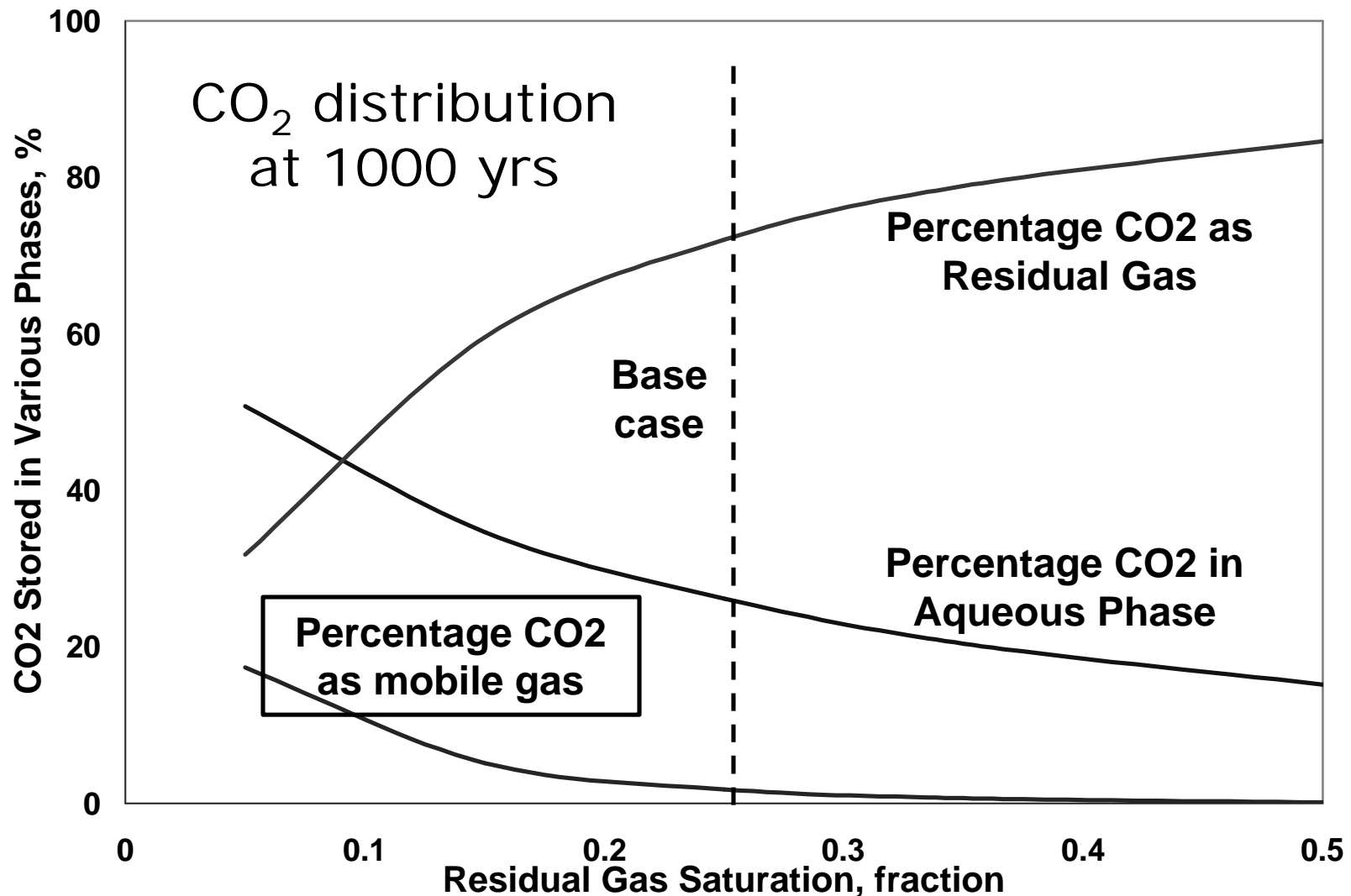
The majority of CO₂ is stored as a residual phase



Key Findings (2):



Even low residual CO_2 saturation leads to residual phase as the dominant mechanism



Key Findings (3):

Well Completion Positioning Can Avoid Seal Integrity Issues

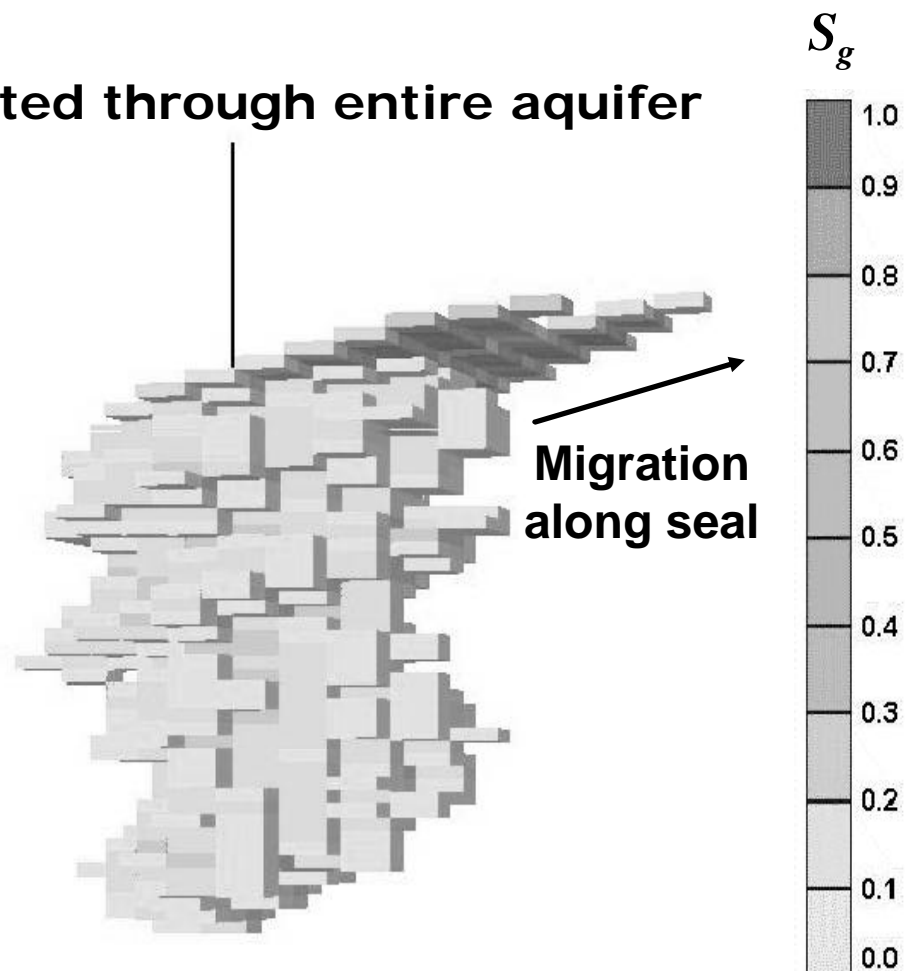


Completion scenario

- **Injection well completed through entire aquifer**

Result

- **Up-dip migration of injected CO₂ for long distances**
- **Increased opportunity for leakage through formation top**



Summary and Conclusions

- After injection ends, capillary effects reduce the amount of mobile CO₂
 - Dissolution into brine
 - Gravity driven flow
- Time required to eliminate mobile CO₂ depends on petrophysical properties of aquifer
 - Residual gas saturation (S_{gr})
 - Average permeability
 - Relative permeability (inc. hysteresis)
 - Anisotropy
- Gas migration is affected most by
 - Dip
 - Anisotropy

Summary and Conclusions

- ❑ Large fractions ($>95\%$) of injected CO_2 can be immobilized in 1000 y
- ❑ Well completion design may significantly reduce the chances of leakage
- ❑ Potential leakage of gas through faults/fractures prior to trapping should be studied in more detail

Extra Slides

Tuning PR-EOS Parameters for CO₂-Brine System



$$BIC_{H_2O-CO_2} = -0.093625 + (4.861E - 4 * (T - 113)) + (2.29E - 7 * S)$$

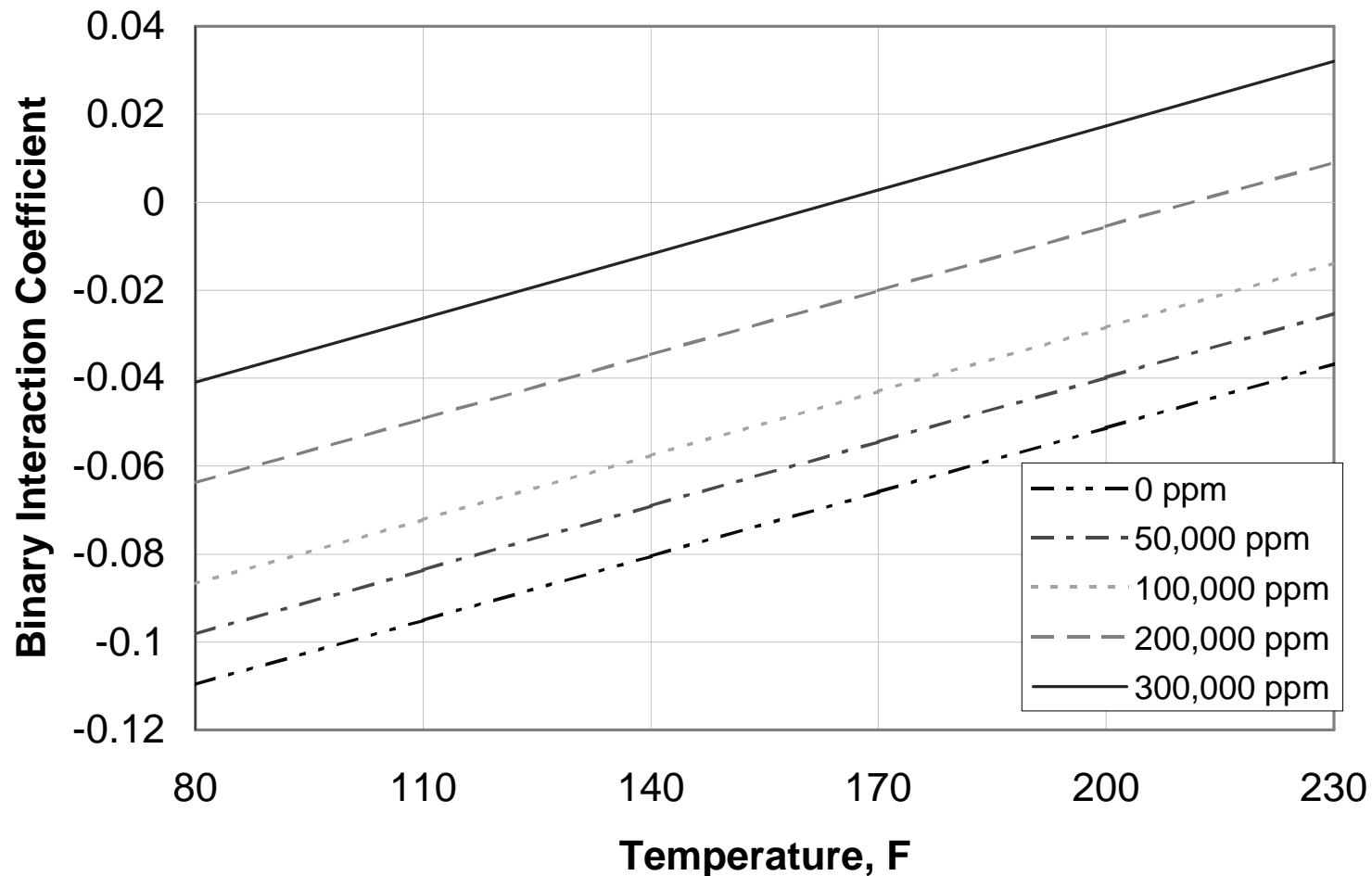
$$VSP_{H_2O} = 0.179 + (2.2222E - 4 * (T - 113)) + (4.9867E - 7 * S)$$

- $BIC_{H_2O-CO_2}$ is Binary Interaction Coefficient for H₂O-CO₂ pair
- VSP_{H_2O} Volume Shift Parameter for H₂O
- T is temperature in degree Fahrenheit
- S is salinity of brine in ppm of NaCl

Tuning Binary Interaction Coefficient for H₂O-CO₂ pair



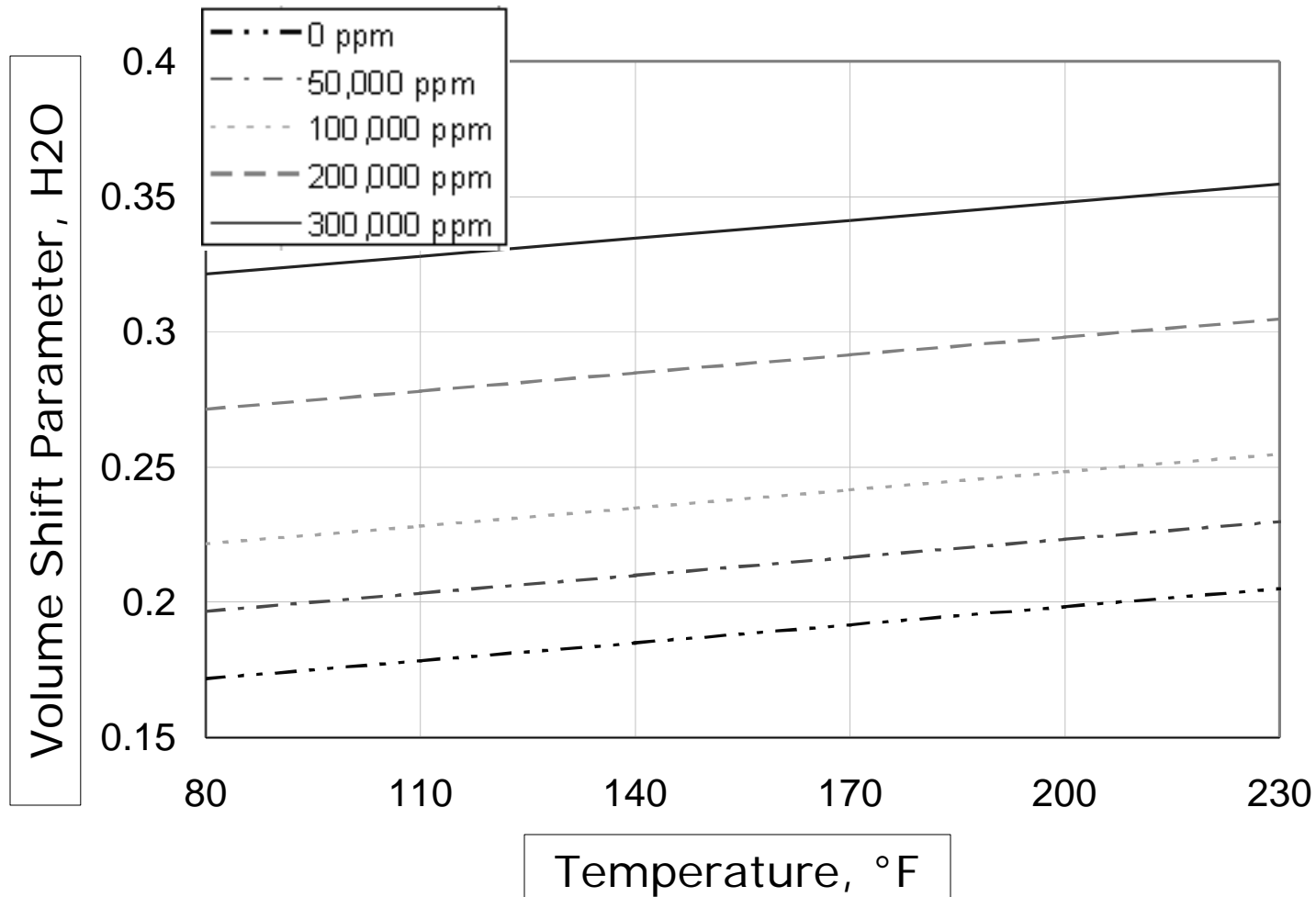
$$BIC_{H_2O-CO_2} = -0.093625 + (4.861E-4 * (T - 113)) + (2.29E-7 * S)$$



Tuning Volume Shift Parameter for H2O

CPGE

$$VSP_{H_2O} = 0.179 + (2.2222E-4 * (T - 113)) + (4.9867E-7 * S)$$



Plot